

## LMG670

#### Precision Power Analyzer



# [Power Analysis]<sup>2</sup> with Dual Path

#### Two Bandwidths Simultaneously

Single-shot results for narrowband, broadband & harmonics measurements

### LMG670 - powerful, convenient, flexible





#### Modular with up to seven power channels





Measurement Channels

#### Setting the bar in power analysis

For more than three decades, ZES ZIMMER has been focused solely on high-precision power measurement technology – so we know there is more to it than simply measuring current and voltage. Anyone who has tried to use generic data acquisition systems for power measurement will have rapidly run up against their limitations. What is the situation with common-mode rejection? Is the result still reliable for power factors in the range of 0.01? Is the earth capacitance low enough to avoid interference by leakage currents? In which frequency ranges does the manufacturer guarantee the stated measuring accuracy? It quickly becomes clear that only a device designed specifically for power measurement can really satisfy these high requirements. The LMG670 from ZES ZIMMER stands out in the market for its extreme reliability, best-in-class accuracy, and maximum frequency range – the ideal prerequisites for excellent results.

#### The right channel combination for every application

Power analyzers are available in different accuracy classes, to allow the user to choose the right tool for the job at hand. After all, not all applications require maximum precision; often lower resolution and frequency range are sufficient. Unfortunately, not all measuring applications exhibit this distinction. It is very well possible, for instance, to have need for different frequency ranges and accuracy levels at different points in the same measurement configuration. This is why the LMG670 offers three different channel types, which can be combined in the same chassis without problems to ensure that you always have a measuring device tailored to your needs for your particular application, without having to accept tradeoffs in accuracy or take a sledgehammer to crack a nut, if a lower priced solution could have served your purposes equally well.



#### Measuring in two bandwidths at the same time, thanks to DualPath - no compromises, no doubts

On conventional power analyzers, a signal first undergoes analog processing, the output values of which are digitized by an A/D converter and then processed. The resulting signal can then either be measured across the whole frequency range, or have antialiasing filters applied to serve as a base for an FFT or further digital filtering. Due to the limitation to a single A/D converter, there are inherently some downsides to be factored in with conventional devices. If measurements are carried out with filters active, in order to avoid aliasing with FFTs, the wideband values are lost. With the filters switched off, strictly speaking, FFTs should not be used. If FFTs are used without an anti-aliasing filter for measurements across the full frequency range, the quality of the calculated values is questionable. An aliasing error of 50%, for instance, is easily detected, however a deviation of 0.5% could go unnoticed. Lastly, when alternating filtered and non-filtered measurements, the validity of the results is equally in question, as this involves the assumption that the signal does not change over time, which is in practice hardly ever the case. In addition, this procedure is particularly time consuming.



In the end, all of the measurement methods presented are merely unsatisfactory compromises. This is why ZES ZIMMER has fundamentally redesigned signal processing and developed the DualPath architecture. The analog side is the same as in conventional measuring devices, however the subsequent digital processing has been revolutionized. The LMG670 is the first power analyzer to have two A/D converters in two independent signal paths for each current and voltage channel. One, for the filterless measurement of the wideband signal, and another, for the narrowband signal at the output of the anti-aliasing filter. The parallel processing of the digitized sample values gives the user access to both measurements of the same signal, without risking aliasing effects. This unique procedure avoids all of the downsides of previous approaches and guarantees the most precise result in the shortest time possible.



#### Gapless measurement

In the course of stricter monitoring of the consumption and efficiency of electrical devices, new standards and procedures are continuously being introduced (e.g. SPECpower\_ssj2008, IEC 62301, EN 50564), in order to enable an impartial comparison of products from different manufacturers. Be it an office computer, server or house-hold appliance, the same principle applies:

the procedure always requires long term analysis of the power consumption, taking into account all relevant operating conditions. The differences between minimum load - e.g. in standby - and full load can be of a significant magnitude, which makes precise measurement very challenging (see also application report no. 102 "Measurement of standby power and energy efficiency" at www.zes.com). Some of the measurements required must be performed over several hours, yet without gaps. By selecting a sufficiently wide measurement range, changing ranges and the inevitably associated losses in data can be avoided. The high basic accuracy of the LMG670 ensures precise measurement results, even near the lower limit of a range.

#### Precise measurements thanks to minimal delay differences

The fast-switching semiconductors used in modern frequency converters to improve efficiency produce extremely steep voltage edges. The resulting capacitive currents put strain on the bearings and the insulation of the motors – this can lead to premature failure.

Motor filters (e.g. dU/dt filters) attenuate the steep voltage gradient, although they generate power losses themselves due to the transient oscillation with the filter's own frequencies (typically > 100 kHz). The broad frequency range and the minimal delay between current and voltage on LMG670's allow extremely precise power loss measurements on the filters at these frequencies, including longitudinal measurements at low power factors. This also applies to power measurements with high frequency ranges of up to 10 MHz, which require the current and voltage channels to be designed for the smallest delay differences. On the LMG670 the offset is less than 3 ns, corresponding to a phase error <1 µrad at 50 Hz. This makes the devices best suited to measure the power losses at low phase angles for transformers, chokes, capacitors and ultrasonic generators. No additional options or adjustments are required; the LMG670 is already fully capable of this measurement task with the standard factory settings. Usually current and voltage transducers are used for measurements on high-power circuits. The phase angle of these transducers can be corrected to improve measurement accuracy.

#### Exact measurements without limits

Although the LMG670 offers unmatched dynamic range, both for voltage and current, there are always applications with extraordinary requirements in terms of measurement ranges. Whether you are dealing with currents of several hundred amps or voltages of several kilovolts, ZES ZIMMER has the right solution at the ready. We offer a wide range of current and voltage sensors, which work perfectly in unison with the LMG670 precision power analyzer and extend the measurement ranges of the device by the required amount. The sensors of our Plug 'n' Measure series are equipped with a bus system, which enables automatic configuration of the LMG670. This allows for all of the important parameters, such as the precise scaling factor, the delay compensation variable, the last calibration date, and the sensor type, to be read automatically by the power analyzer and taken into account during measurements. Moreover, the sensors are actively supplied with power by the LMG670, separate power supplies are no longer required.

With Plug 'n' Measure there is no need for fine tuning by the user to achieve the best possible results. From the user's perspective, there is no difference between direct and sensor-supported measurements. Of course, other commercially available sensors can also be used with the LMG670.



Sensor Type PCT

#### Powerful interfaces

In addition to the GUI and the connection to the device under test itself, the exchange of data with the existing computer and software environment is of primary importance in determining how well the instrument is able to perform its intended task. Only with seamless integration into the overall system can the full power of the instrument be harnessed by the user. The high sampling rate of the LMG670 inevitably creates a large amount of data. Therefore we have ensured, by using the right system architecture, that the measured data can be transmitted via the interfaces at a high throughput rate. Even high-resolution measurements of all important parameters such as current, voltage, active power, et cetera over a period of several minutes can be rapidly transferred to a connected computer. In order to cope with the requirements of a wide array of different applications, a range of ports is available. In addition to a serial port and Gigabit Ethernet, a slot is available for USB 2.0; the device can also optionally be equipped with a VGA/DVI output for connecting an external monitor or projec-

tor. Two more slots can be retrofitted for future interface standards. By using the integrated sync interface, it is possible to precisely synchronize multiple LMG670's with one another. This makes it possible to have a common time base for measurements involving multiple LMG670's on the same system, or the mutual connection and control of an LMG670 by oscilloscopes or waveform generators. Thanks to its internal HDD, the LMG670 provides the option to store measured values, settings, user-defined measurement variables, or graphs for later use, even without having a PC connected. When it comes to storage capacity, the customer has several options available. The firmware of the LMG670 can be quickly and easily brought up to date via USB.



#### Process signal interface

It is often necessary to take further measurements in addition to electrical parameters to be able to make a meaningful overall statement on the performance and efficiency of the device being tested. Hence, it is vital to be able to perfectly synchronize these measured values with the RMS values calculated by the LMG670, in order to establish reliable timing between electrical and mechanical events. A typical application is the analysis of electrical drive systems, where torque and speed must be measured and reconciled with the electrical parameters. Conversely, it may also be necessary for the power analyzer to output results for further processing in analog form, or to trigger switching operations depending on measured variables or derived values. In order to be equipped for all of these potential requirements, the LMG670 offers a multitude of different input/output features for analog and digital signals.

2 fast, synchronized analog inputs (ca. 150 kS/s)
8 analog inputs
8 switching inputs (ca. 150 kS/s)
2 torque-/speed-/ frequency inputs
32 analog inputs
8 switching outputs

#### Star-to-delta conversion

In three-phase three-line systems, only the line-to-line voltages  $V_{12}$ ,  $V_{23}$ ,  $V_{31}$  and the line currents  $I_1$ ,  $I_2$ ,  $I_3$  are accessible for measurement. With the star-to-delta conversion option, the line-to-line voltages can be converted to non-accessible phase voltages and the related active power can be determined. Likewise the line currents can be converted into "linked" currents. From these calculated values it is possible to derive all other variables, such as

harmonics. Distortions and imbalances of the grid or consumers are properly taken into account. This makes the use of an external, artificial neutral point superfluous; although one could use one at any time, provided that the associated disadvantages (e.g. increased power losses) are taken into account.



3-phase 3-wire system: measuring phase-to-phase voltage and line currents

#### Easy to use – with or without touchscreen

To ensure that the LMG670 can be used in all conditions, particular attention has been paid to universal usability. All display modes and setting options can be operated both by the touchscreen or the keypad, without exception. The optimized design consistently links the keypad to the associated views and setting options on the screen. To use the instrument effectively requires almost no familiarization. The graphical user interface directs the user without detours to the required values. Be it RMS of voltage or current, associat-

ed harmonics or cumulative values, these are usually only a single press of a button away. In addition, user-defined views allow to group individually measured values, so that all the parameters are always available at a glance. This ergonomic way of operation and the associated time savings contribute directly to the productive use of the LMG670. The eight context-specific double softkeys to the right of the display, whose function always corresponds to their onscreen counterparts on the right-hand side, are especially important for ease-of-use.

One can determine the function assigned to a given softkey at a glance. The double softkey design enables the respective parameter to be rapidly configurable; switching through views that are not relevant is no longer necessary. Should there be questions as to function and control while operating the device, the relevant sections of the manual can be displayed at any time.



Simultaneous measurement of narrow and broadband values



Display of measured RMS values



Display of sampling values of 8 signals in two scopes

#### Everything important just a click away

										Harmoni
Uthe	1	08.315		Ithd	2.487		Ph	1.665		Transfor
		4.206	var	Q <sub>tot</sub>	6.531	var	D	4.99697	var	*
		6.740		φ <sub>fund</sub>	69.3837		$\mathbf{f}_1$	19.7826		Phase - I
		9.7826								1
		U 1							P 1	Harmoni
0	.071				0.453 mA			-0.000		Odd & Ev Values
					8.634 mA			1.609		U
	. 294				0.446 mA			0.000		
	.056				0.331 mA			-0.000		
	.063				0.288 mA			0.000		
	.067				0.083 mA			0.000		
	р. 1 ЦАЈА . 77 — На				Grp. 2 1.542 kH				Grp. 3	$\rightarrow$

							Normal
	21.4663		21.4486		21.4586 W	64.3734 W	Transform
	35.0092	VA	34.9769		34.9960 VA	104.982 VA	×
	27.6558	var	27.6286	var	27.6451 var	82.9296 var	Phase / Ch
PF	0.61316		0.61322		0.61317	0.61318	All
U <sub>trms</sub>	208.122		208.366		208.243 V	360.689 V	Bandwidth
$U_{\text{de}}$	0.013		-0.178		-0.823 V		
U <sub>ac</sub>	208.122		208.366		208.242 V		Values
I <sub>trms</sub>	168.215	mA	167.862	mA	168.054 mA	291.060 mA	Many
	0.788	mA	1.312	mA	1.992 mA		
lac	168.213	mA	167.857	mA	168.042 mA		
f <sub>cycle</sub>	49.9971		49.9971		49.9971 Hz	49.9971 Hz	
	1.23724	kΩ	1.24129	kΩ	1.23915 kΩ		
role 50	0.0 ms Grp. 1 UA				Grp. 2 Direct 50.00 Hz	Grp. 3 Direct 50.00 Hz	$\vdash$

Click on the <Phase-Ch> softkey: measured values for all channels or linked values in a group

Gro. 3

3.0

Display Normal Transform

Phase - Ch

Bandwidth

Values

Click on softkey <Display>: toggling between RMS values and harmonics



*Click on* Cycle: *Configuration of cycle time or reference* 

Click on the group: configuration of activation, synchronization, filters, etc.

Group 1 Group 2 Group 3 Sums

69.585

89.057 mA

1.658

6.197

0.26762

V

W

ind

VA

**Grp. 2** 1.658 kHz

U<sub>trms</sub>

trms

Ρ

PF

S

Cycle

Click on the level indicator: configuration of channel-specific measurement ranges and sensor settings

	Signal				Table Signal
		f <sub>cycle</sub>	19.7652 Hz		Wiring
	AC+DC				
		Bandwidth			Signal E Coupling
					AC+DC
					Harmonics
		Low-pass			Interharm. Č
Wideband Filt.		High-pass			
					Processing
					Dual Path
					Filter
yole Freeze Grp. 1 W		Grp. 2		Grp. 3	$\succ$

				Group
Auto Range	Auto	Auto		Channel
				1
				Select I/U
Range				U Auto Rangi
				Auto
Auto Range	Auto	Auto	Auto	Jack U*
				Sensor
Sensor				Default
Range				Range
				400.0 V

#### Clear visualization of measurements thanks to groups

In order to properly illustrate the functional relations between physical measurement channels, the power measurement channels (P-channels) can be organized into so-called groups, which appear almost as virtual measurement channels or virtual devices in addition to the physical channels. The logical grouping of the P-channels is dependent on the number of wires and phases of the electrical system being analyzed. Thanks to the flexibility of the LMG670, it is possible to model even unusual and rarely seen configurations, such as split-phase systems and four-phase or multiphase systems, both simply and reliably. The only requirement is that all of the channels within a group have the same basic frequency and are of the same type (A1, B1, C1). This will avoid subtle errors, which arise due to the different technical properties of the different channel types. One benefit of creating groups is that it makes configuring the device easier, since filter settings (for example) affecting all channels in the group only have to be configured once. In addition, derived values, such as active, apparent or idle power are calculated across all channels in the group. While grouping specifies how the channels are combined logically, the wiring dictates how the inputs of the measuring device are connected to the measuring circuit, i.e. whether it is a star-to-delta circuit or whether there are neutral wires, etc. The wiring defines how the measured signals are interpreted by the device.



*Example: measurement on frequency converter* 

Group I measures the input power in an Aron circuit. C1-channels are usually sufficient.

To determine the output power, Group II measures the voltages on the delta side and the currents on the star side. A1-channels are recommended for this. Using another singlechannel group, the DC intermediate circuit can also be measured. A1-channels would also be indicated here.



Logical grouping of channels for different points of measurement in the LMG670 configuration menu

#### Electrical drive systems

Frequency converter

DC

AC

3)

A/B channel

More than half of the electrical energy generated worldwide is converted to mechanical motion, and the importance of electric powertrains for transport of goods and people is growing steadily. While outdated speed controllers are afflicted with losses of up to 40%, modern, frequency-controlled systems can achieve efficiency levels of over 95%. These frequency convert-

AC

2-4

C channel

1)

DC

2)

A/B channel

ers use pulse width modulation to control the speed of the motor with hardly any losses. The objective is to optimally adjust the converter and motor to one another, in order to achieve the best overall efficiency. Measuring the input power, the intermediate circuit, and the output power of the converter as well as the mechanical power of the motor simultaneously is anything

Μ

but trivial. In addition to the integration of sensor technology (wideband sensors for high currents, high-voltage dividers, precise speed and torque transmitters), the instrument must meet the challenge of measuring the very steep-flanked signals at the converter output. This environment is often described as harsh, not merely from an EMC point of view.

Determining the efficiency of an electric drive system

- 1) Input of the converter: C1-channels are usually sufficient for this.
- 2) DC intermediate circuit: depending on the required level of precision, A1 or B1-channels are required, as the DC intermediate circuit exhibits significant residual ripple under certain circumstances.
- 3) Converter output: depending on the required level of precision, A1 or B1-channels only are to be used.
- 4) Measurement of mechanical quantities synchronously to 1) 2) 3) 4) up to 150kS/s via process interface

band power, and another one on a filtered signal to determine the power at certain frequencies, resp. a subsequent FFT analysis to measure the harmonic spectrum. This procedure is very time-consuming, yet it cannot guarantee that the conditions present during the initial measurement still prevail during the repetition.

The innovative DualPath architecture of the LMG670 provides all of the required results simultaneously in a single measurement, with maximum precision, and the widest frequency range on the market - free from aliasing effects.





Of course the key question in the analysis of electrical drive systems is: which part of the electrical energy at the converter output relates to the torque-relevant fundamental frequency of the motor, and which

part to the remaining frequency range, particularly the harmonic spectrum? To give an accurate answer, it has long been necessary to perform two separate measurements: one without filters to establish the wide-



4)

M, Mn

Scope display of the voltages at the converter output. The wideband values (\_\_\_\_\_) show the PWM signal, the narrowband values (\_\_) are sinusoidal.



#### Switched-mode power supplies

Already years ago, advances in power electronics have caused relatively large and heavy transformer power supplies to be replaced by smaller, lighter and more efficient switched mode power supplies. Today those can be found in practically all grid-powered electrical devices. While avoiding many of the downsides of their predecessors, they also bring new challenges: for one, the conducted emissions due to harmonics are not insignificant and must be limited by standards (EN61000-3-2, EN61000-3-12). Secondly, the high switching frequencies of up to several hundred kilohertz can lead to problems with electromagnetic compatibility, both on the grid side and on the consumers' part. The role of power measurement technology is to support the manufacturer in optimizing their products.



#### Solid & laminated magnetic cores

Under the influence of changing fields, the ferromagnetic components of an electrical machine are subject to losses due to continuous remagnetization and eddy currents, which are ultimately converted into heat or vibrations.

The total losses are frequency-dependent and should be minimized as far as possible, as

they have a significant effect (for example) on the range of the batteries in electric vehicles. The core power loss can be calculated directly from the excitation current of a test winding and the magnetization voltage of a sensor winding. The magnetic flux density in the core material can be derived from the rectified value of the voltage induced in the sensor winding. The magnetic field strength is proportional to the current flowing in the test winding.

While the high-frequency currents in solid cores can be measured directly, the high amp values occuring in laminated cores usually demand high-precision transducers.



- Precise determination of the active power, even at lowest power factors ( $\lambda$  < 0.01) and very low voltages
- Calculation of a multitude of derived variables such as peak value of field strength ( $H_{pk}$ ), magnetic flux density ( $B_{pk}$ ), and amplitude permeability ( $\mu_a$ )
- Convenient integration of transducers for high currents



#### Conformance testing for the aerospace industry

Particularly in the aerospace industry, electromagnetic compatibility between installed systems is of existential importance. For this reason, industry directives such as ABD0100.1.8 set limits on harmonic currents up to the range of 150 kHz. These harmonics can be analyzed using the LMG670. This can either be accomplished using the built-in harmonics analysis, or alternatively in any level of detail via offline analysis of sample values using external software.



#### Lighting technology

In an effort to reduce energy consumption, light bulbs are being replaced with ever more efficient light sources all around the world. While on the consumer end all that is required is to insert a new product into the existing fitting, the differences on the electrical level are considerable – in contrast to conventional bulbs, LED lights and compact fluorescent lights ("low-energy light-bulbs") are controlled by special electronic ballasts. Some of these ballasts work with switching frequencies of up to 200 kHz and produce signal distortions at frequencies of up to 1 MHz. The manufacturers are required first and foremost to prevent damaging circuit feedback, and secondly, to ensure optimum service life for their products. To achieve the aforementioned objectives, often a controlled warm start is performed, whose proper execution has to be verified by making appropriate measurements.



- Broad frequency range of the measurement, hand-in-hand with a high level of precision
- Verification of standby power of ballasts even for  $\lambda$  < 0.01
- Minimal earth capacitance to avoid leakage currents during the measurement



#### CE compliance testing for harmonics and flicker

Electrical equipment, systems and devices must satisfy the directives and ordinances of the EU on the permitted level of electromagnetic emissions and immunity to electromagnetic effects, if they are put on the market inside the European Union (EU). Two different types of grid emissions are tested: harmonics and flicker. Any electrical device with a non-linear load characteristic produces current harmonics. Due to the impedance of the grid, these cause drops in voltage and resulting distortions. In addition, certain devices (e.g. continuous-flow heaters, heating furnaces, et cetera) control their power consumption by abruptly switching on and off, which destabilizes the voltage level due to the grid impedance. This produces fluctuations in voltage, which trigger variations in brightness in the electric lighting ("flicker"). In combination with a suitable AC source and reference impedance, the LMG670 is the tool of choice for the qualified assessment of harmonics and flicker. The LMG Test Suite (see accessories) is providing a user-friendly software solution for this, which turns performing conformity tests for electromagnetic compatibility into child's play.



#### Technical Data (Summary)

A1 channel				± (% of I	neasured value +	% of maximum	ı peak value)			
Accuracy	DC	0.05 Hz 45 Hz 65 Hz 3 kHz	45 Hz 65 Hz	3kHz 10kHz	10 kHz 50 kHz	50 kHz 100 kHz	100 kHz 500 kHz	500 kHz1 MHz	1MHz 2MHz	2 MHz 10 MHz
Voltage U*	0.02+0.08	0.015+0.03	0.01+0.02	0.03+0.06	0.2	+0.4	0.5+1.0	0.5+1.0	f/1MHz*1.5	+ f/1MHz*1.5
Voltage U <sub>SENSOR</sub>	0.02+0.08	0.015+0.03	0.01+0.02	0.03+0.06	0.2-	0.2+0.4		0.4+0.8	f/1MHz*0.7	+ f/1MHz*1.5
Current I* 5mA5A	0.02+0.1	0.015+0.03	0.01+0.02	0.03+0.06	0.2-	0.2+0.4		0.5+1.0	f/1 MHz*1.0 + f/1 MHz*2.0	-
Current I* 10A32A	0.02+0.1 <sup>1)</sup>	0.015+0.03 <sup>3)</sup>	0.01+0.02 <sup>3)</sup>	0.1+0.2 <sup>3)</sup>	0.3+0.6 <sup>3)</sup>	f/100kHz*0	.8 + f/100 kHz*1.2 <sup>3)</sup>	-	-	-
Current I <sub>sensor</sub>	0.02+0.08	0.015+0.03	0.01+0.02	0.03+0.06	0.2-	+0.4	0.4+0.8	0.4+0.8	f/1MHz*0.7	+ f/1MHz*1.5
Power U*/ I* 5mA5A	0.032+0.09	0.024+0.03	0.015+0.01	0.048+0.06	0.32	2+0.4	0.8+1.0	0.8+1.0	f/1MHz*2.0 + f/1MHz*1.8	-
Power U*/ I* 10A32A	0.032+0.09 <sup>2)</sup>	0.024+0.034)	0.015+0.014)	0.104+0.134)	0.4+0.54)	f/100kHz*0.8 f/100kHz*0.8		-	-	-
Power U*/ I <sub>sensor</sub>	0.032+0.08	0.024+0.03	0.015+0.01	0.048+0.06	0.32	2+0.4	0.72+0.9	0.72+0.9	f/1MHz*1.8	+ f/1MHz*1.5
Power U <sub>sensor</sub> / I* 5 mA5 A	0.032+0.09	0.024+0.03	0.015+0.01	0.048+0.06	0.32	2+0.4	0.72+0.9	0.72+0.9	f/1MHz*1.4 + f/1MHz*1.8	-
Power U <sub>SENSOR</sub> / I* 10 A32 A	0.032+0.09 <sup>2)</sup>	0.024+0.034)	0.015+0.014)	0.104+0.134)	0.4+0.54)	f/100kHz*0.8 f/100kHz*0.8		-	-	-
Power U <sub>SENSOR</sub> / I <sub>SENSOR</sub>	0.032+0.08 0.024+0.03 0.015+0.01		0.048+0.06	0.32+0.4		0.64+0.8	0.64+0.8	f/1MHz*1.1	+ f/1MHz*1.5	
B1 channel				± (% of 1	neasured value +	% of maximum	ı peak value)			
Accuracy	DC	DC 0,05 Hz 65 Hz		45 Hz 65 Hz	1kHz.	5 kHz	5 kHz 20 kHz	20kHz 1	00kHz	100 kHz 500 kHz
Voltage U*	0.1+0.1	(	0.1+0.1	0.05+0.05	0.2+0.2		0.3+0.4	0.4+0.	8 1 1	100kHz*0.8 + /100kHz*1.2
Current I* 5 mA5 A Current I <sub>SENSOR</sub>	0.1+0.1	(	0.1+0.1	0.05+0.05	0.2+0.2		0.3+0.4	0.4+0.	X I I	100kHz*0.8 + /100kHz*1.2
Current I* 10 A32 A	0.1+0.1 <sup>1)</sup>	0	.1+0.1 <sup>3)</sup>	0.05+0.05 <sup>3)</sup>	0.05+0.05 <sup>3</sup> ) 0.2+0.2		0.6+1.23)	1.5+1.	5-/	100kHz*2.0 + /100kHz*2.0 <sup>3)</sup>
Power U*/ I* 5 mA5 A Power U*/ I <sub>SENSOR</sub>	0.16+0.1	0	.16+0.1	0.07+0.04	0.32+0.2		0.48+0.4	0.64+0		100 kHz*1.28 + /100 kHz*1.2
Power U*/ I* 10 A32 A	0.16+0.1 <sup>2</sup>	0.	16+0.14)	0.07+0.044)	<sup>4)</sup> 0.32+0.2 <sup>4)</sup>		0.72+0.84)	1.52+1.	154)	1 00 kHz*2.24 + /1 00 kHz*1.64)
C1 channel				± (% of n	neasured value +	% of maximur	n peak value)			
Accuracy	DC		Hz 45 Hz z 200 Hz	45 Hz 65 Hz	200Hz .	500 Hz	500 Hz 1 kHz	1 kHz 3	2 kHz 2	kHz 10 kHz
Voltage U*	0.1+0.1	0.	02+0.05	0.02+0.02	0.05	+0.05	0.2+0.1	1.0+0	.5	f/1kHz*1.0 + f/1kHz*1.0
Current I*	0.1+0.1 <sup>1)</sup>	0.0	02+0.05 <sup>3)</sup>	0.02+0.02 <sup>3)</sup>	0.05+	+0.05 <sup>3)</sup>	0.2+0.1 <sup>3)</sup>	1.0+0.		f/1kHz*1.0 + f/1kHz*1.0 <sup>3)</sup>
Current I <sub>sensor</sub>	0.1+0.1	0.	02+0.05	0.02+0.02	0.05	+0.05	0.2+0.1	1.0+0		f/1kHz*1.0 + f/1kHz*1.0
Power	0.16+0.1 <sup>2</sup>	0.0	32+0.05 <sup>4)</sup>	0.03+0.01 <sup>4)</sup>	0.08+	+0.054)	0.32+0.14)	1.6+0.		f/1kHz*1.6 + f/1kHz*1.0 <sup>4)</sup>
Accuracies valid for:	2. 3.		cure (23±3) °C Ik value for power	r is the product of r kimum peak value f			<ol> <li>6. Current a 10%</li> <li>7. Adjustme</li> </ol>	1 (power factor) nd voltage 110% of nominal ent carried out at on interval 12 mor	23 °C	
Other values		All othe	r values are calcu		. voltage and power $g. S = I * U, \Delta S /$		sp. error limits are de	rived according to	context	

<sup>(1) (2) (3) (4)</sup> only valid in range 10 ... 32 A: <sup>(1)</sup> additional uncertainty  $\pm \frac{50 \mu A}{A^2} * I_{ums^2}$  <sup>(2)</sup> additional uncertainty  $\pm \frac{50 \mu A}{A^2} * I_{ums^2} * U_{trms}$  <sup>(3)</sup> additional uncertainty  $\pm \frac{30 \mu A}{A^2} * I_{ums^2} * U_{trms}$ 

Voltage measuring ranges U*														
Nominal value (V)	3		6	12.5	25		60	130	2	250	400	600	)	1000
Max. trms value (V)	3.3		6.6	13.8	27.5	;	66	136	2	270	440	660	)	1000
Max. peak value (V)	6		12	25	50		100	200		400	800	160	0	3200
Overload protection						1000V +	10% perma	nently, 1500	V for 1s					
Input impedance							4.59 M	Ω, 3 pF						
Earth capacitance							< 9	0 pF						
Current measuring ranges I*														
Nominal value (A)	0.005	0.01	0.02	0.04	0.08	0.15	0.3	0.6	1.2	2.5	5	10	20	32
Max. trms value (A)	0.0055	0.011	0.022	0.044	0.088	0.165	0.33	0.66	1.32	2.75	5.5	11	22	32
Max. peak value (A)	0.014	0.028	0.056	0.112	0.224	0.469	0.938	1.875	3.75	7.5	15	30	60	120
Input impedance	ca. 2.	2Ω		ca. 600 mΩ			ca. 80 mΩ			ca. 20 mΩ			ca. 10 mΩ	!
Overload protection permanent (A)				LMG in ope	eration 10 A						LMG in op	eration 32A		
Overload protection short-time (A)							150 A fo	or 10 ms						
Earth capacitance							< 9	0 p F						
Sensor inputs U <sub>SENSOR</sub> , I <sub>SENSOR</sub>														
Nominal value (V)	0.03		0.06		0.12		0.25	0.5		1		2		4
Max. trms value (V)	0.033	3	0.066		0.132	(	0.275 0.55			1.1		2.2		4.4
Max. peak value (V)	0.097	7	0.1953		0.3906	0.7813 1.563		3	3.125		6.25		12.5	
Overload protection		I		I		100	V permanen	tly, 250V fo	' 1s					
Input impedance							100 kΩ	l, 34 pF						
Earth capacitance							< 9	0 p F						
Isolation	All current Max. 1000	-			jainst each o	ther, agair	st remainin	g electronics	and agains	st earth.				
Synchronization		urable filte		-	period. The p re very stable									
Scope function	Graphical d	isplay of s	ample value	es over time	in two scope	s with 8 s	gnals each							
Plot function	Two time (t	rend-) dia	grams of m	ax. 8 parame	ters, max. re	solution 3	0 ms							
External graphics interface (L6-OPT-DVI)	VGA/DVI in	terface for	external so	creen output										
Process signal interface (L6-OPT-PSI)	8 analog in 32 analog o 8 switching 8 switching	GA/DVI interface for external screen output fast analog inputs (150 kS/s, 16 bit, BNC) analog inputs (100 S/s, 16 bit, D-Sub:DE-09) 2 analog outputs (output per cycle, 14 bit, D-Sub: DA-15 & DB-25) switching outputs (6 switches with 2 connections each and 2 switching outputs with common negative, D-Sub: DB-25) switching inputs (150 kS / s, in two groups 4 inputs each with common ground, D-Sub: DB-25) peed-/torque-/frequency inputs (150 kS/s, D-Sub: DA-15)												
Star-delta conversion (L6-OPT-SDC)	Conversion	of line vol	tages to pl	ase voltages	and comput	ation of re	sulting activ	ve power						
Harmonics at device level (L6-OPT-HRM)	Harmonics a	and interha	armonics up	to 2,000th	order									
Flicker (L6-OPT-FLK)	According t	o EN 6100	0-4-15											
LMG Remote	LMG600 exp	pansion so	ftware, bas	ic module fo	r remote con	figuration	and operatio	n via PC						
L60-TEST-CE61K	LMG600 sof	tware for o	conformity	tests accord	ing to EN610	00 for har	monics and f	licker						
Miscellaneous Dimensions Weight Protection class Electromagnetic compatibility Temperature Climatic category Line input	Depending EN 61010 ( EN 61326 0 40 °C (	on installe IEC 61010 (operation) ironmental	d options: VDE 0411) ) / -20 5 L conditions	max. 18.5 kg ), protection 60 °C (storag s according t	class I / IP2 e)				(WxHxD) 84	HP x 4 RU 3	x 590 mm			

#### Accessories program (excerpt)

Current senso	rs							
Туре		Ring-type :	transducers		Current	clamps	Flexible	Shunt
						0	0.	1000
Name	PCT	L60-Hall	LMG-Z601	LMG-Z5xx	LMG-Z406, L45-Z10/16	L45-Z26	L60-Flex	LMG-SH (-P)
Signal type	AC-	+DC	A	íC	AC	AC+DC	AC	AC+DC
Current ranges	602000 A <sub>eff</sub>	502000 A <sub>eff</sub>	100 A <sub>eff</sub>	100 A <sub>eff</sub>	40 A 3 kA <sub>eff</sub>	30 A 1 kA <sub>eff</sub>	500 A 3 kA <sub>eff</sub>	37mA0,6A <sub>eff</sub>
Best accuracy	0.015%	0.3%	0.15%	0.02%	0.1%	1.5 %	2 %	0.15%
Max. bandwidth	0 Hz1 MHz	0 Hz 150 kHz	30 Hz1 MHz	5 Hz 15 kHz	2 Hz 50 kHz	0 Hz2 kHz	10 Hz5 kHz	4565 Hz
Power supply by LMG670	Y	es	Not re	quired	Y	es	Not re	quired
Plug 'n' Measure	Y	es	N	lo		Yes		No

High-voltag	ge divider	S									
	A 2 2002 Mark Barry Mark Bar										
Name	HST-3	HST-6	HST-9	HST-12							
Signal type		AC+	⊦DC	AC+DC							
Signal type											
Max. voltage	3.15 kV <sub>eff</sub>	$6.3  kV_{eff}$	$9.45  kV_{eff}$	12.6 kV <sub>eff</sub>							
	3.15 kV <sub>eff</sub>	6.3 kV <sub>eff</sub> 0.0		12.6 kV <sub>eff</sub>							
Max. voltage	3.15 kV <sub>eff</sub>		5%	12.6 kV <sub>eff</sub>							
Max. voltage Best accuracy	3.15kV <sub>eff</sub>	0.0	5% 300kHz	12.6 kV <sub>eff</sub>							

Breakout box				
			6	
Name	LMG-MAS	LMG-MAK1	BOB-CEE3-16	BOB-CEE3-32
Nominal voltage	250 V	300 V	230/	400 V
Category	CA	T III	CAT	T II
Safety standard	IEC / E	N61010-1	IEC / EN	61010-1
Socket for load connection	16 A 250 V CEE 7/4	10 A 250 V IEC 60320-C14	16 A 400 V 3L+N+PE, 6 h IEC 60309	32 A 400 V 3L+N+PE, 6 h IEC 60309

The Breakout Boxes enable access to the individual lines in a connector for measurement, and provides an easy and elegant way to take measurements on single and threephase consumers.





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